

Graph Comparing Theoretical and Measured Frictional Torques for Rolling Element Bearings rotating in Planetary Motion

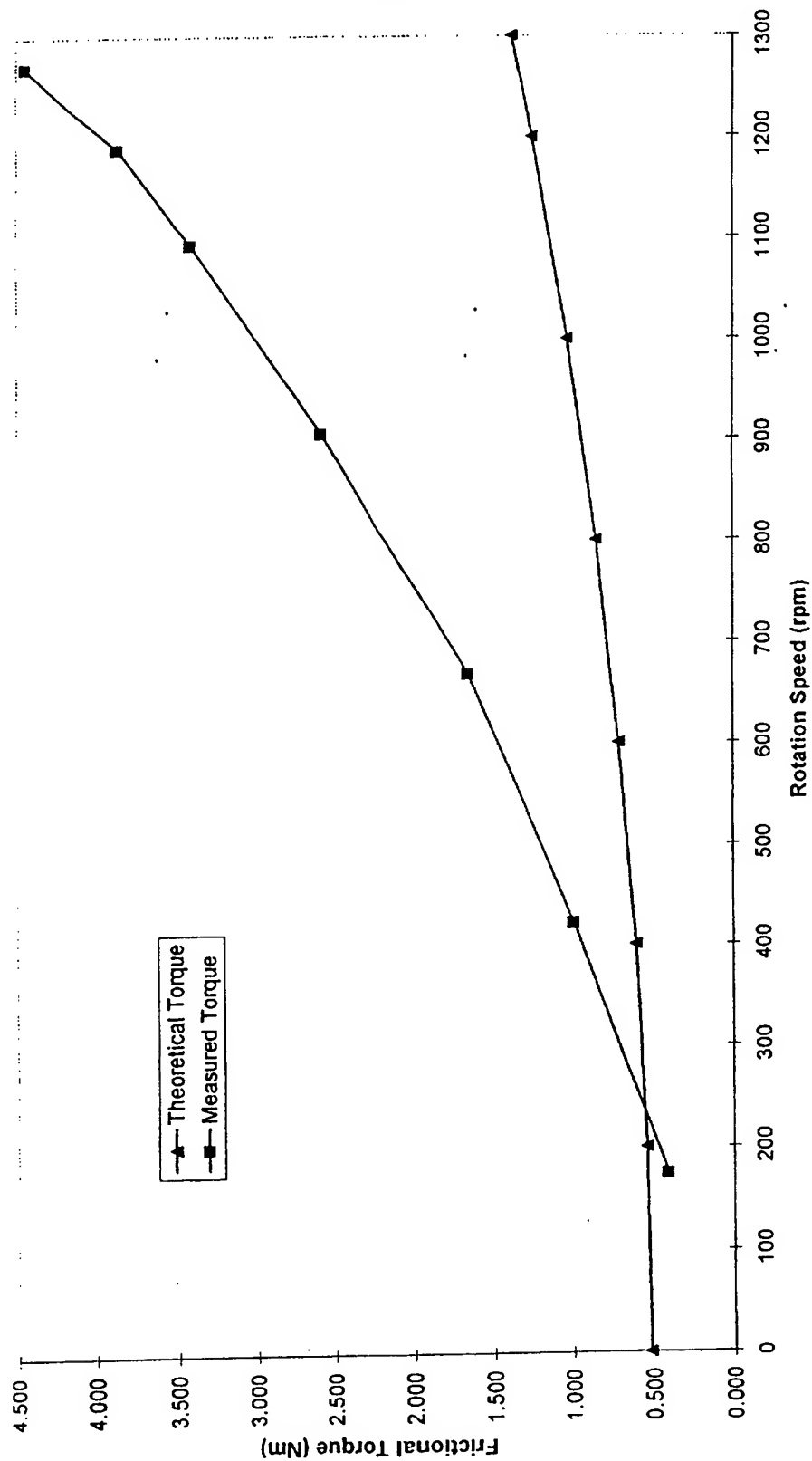


Figure 1

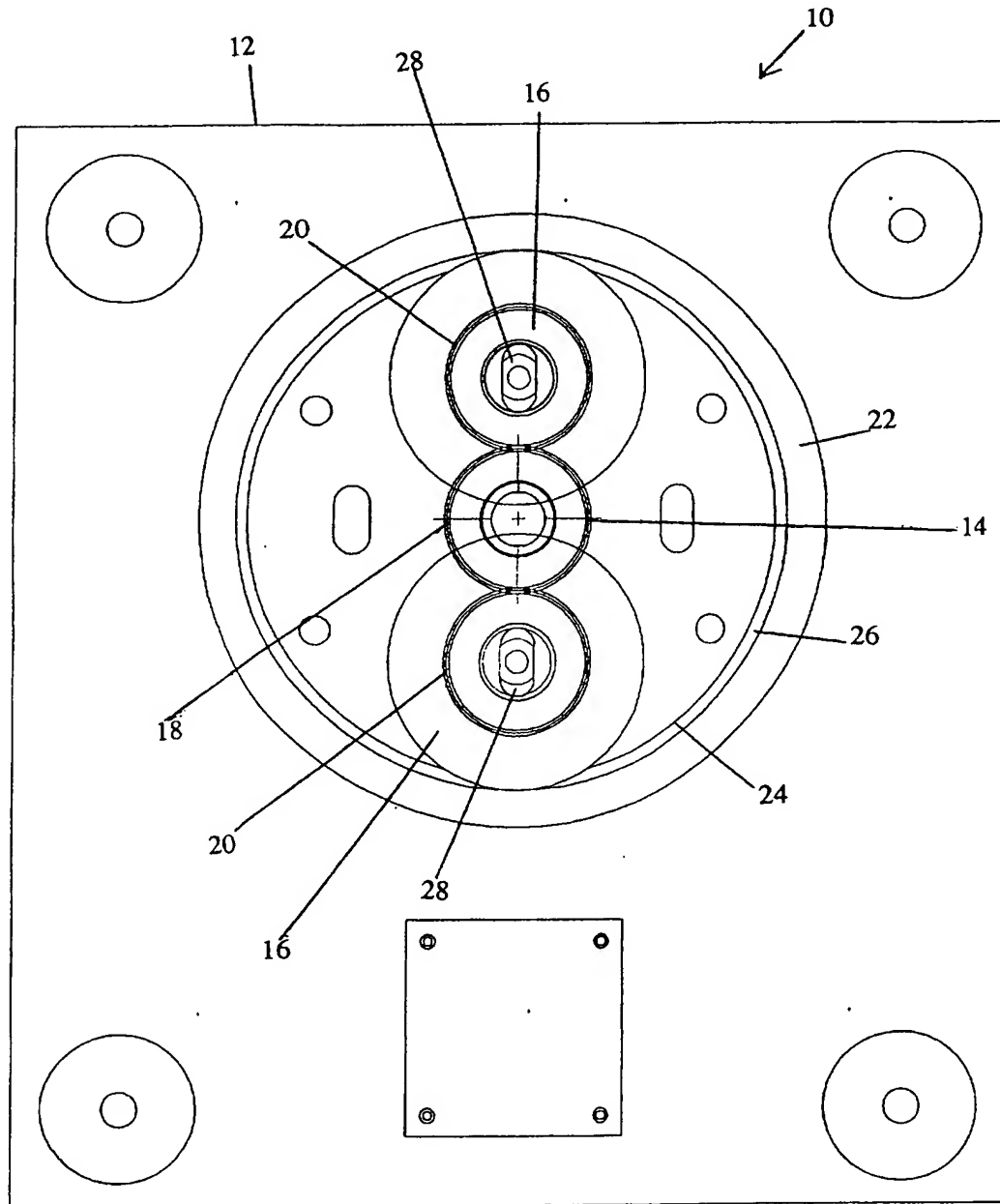


Figure 2

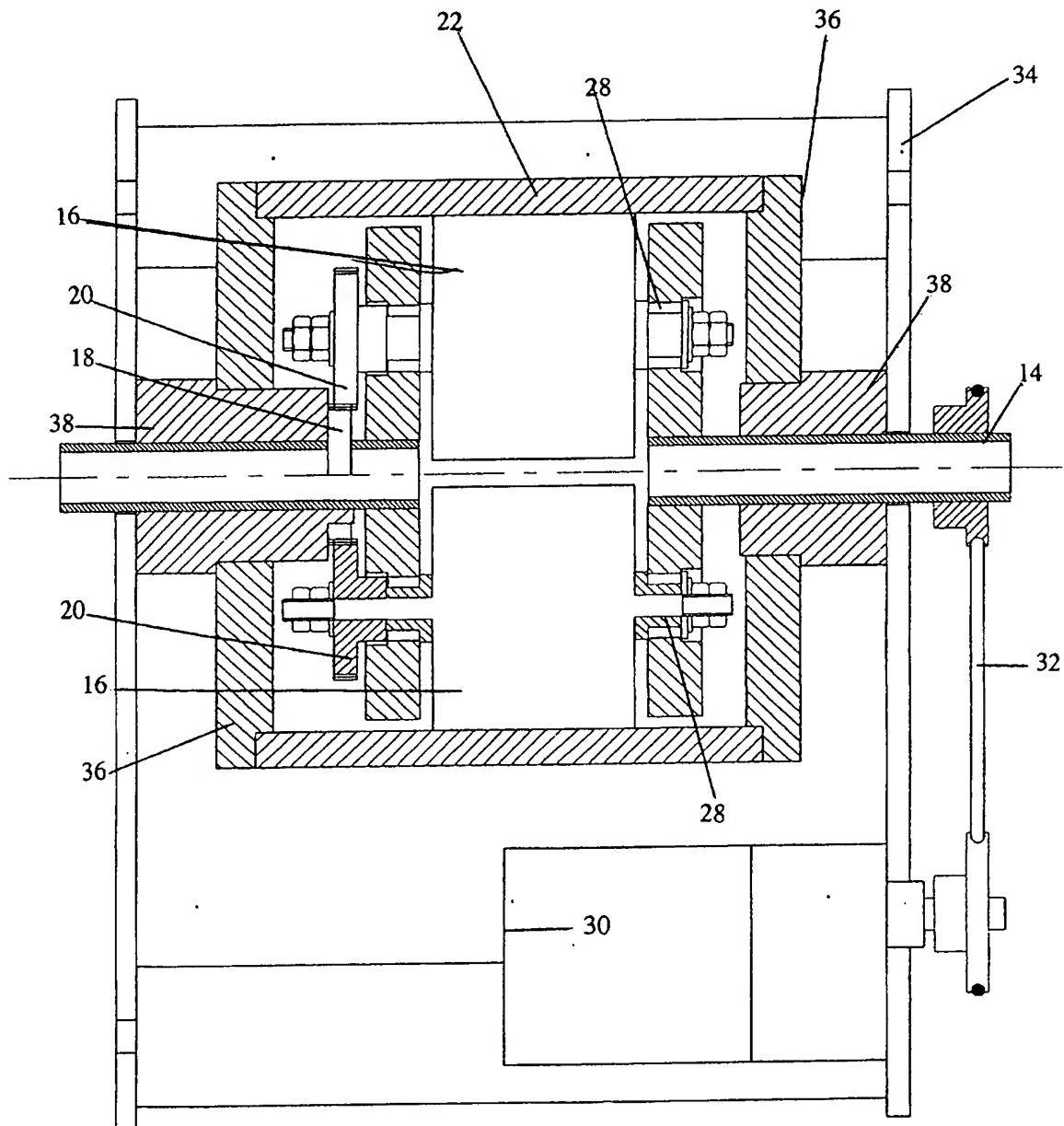


Figure 3

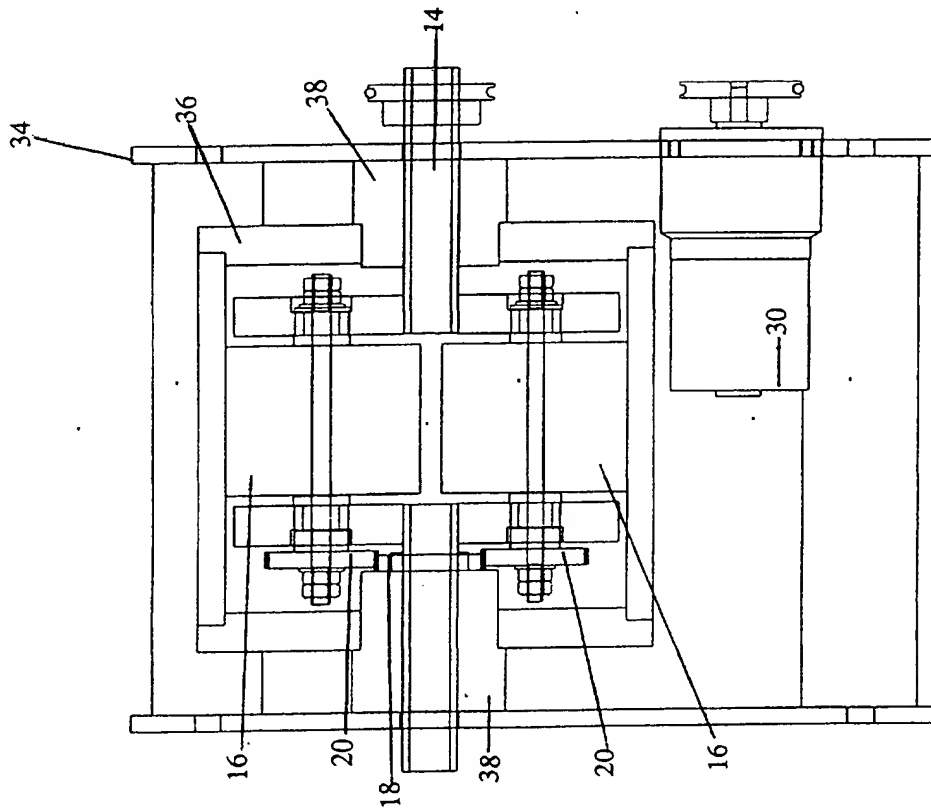


Figure 4

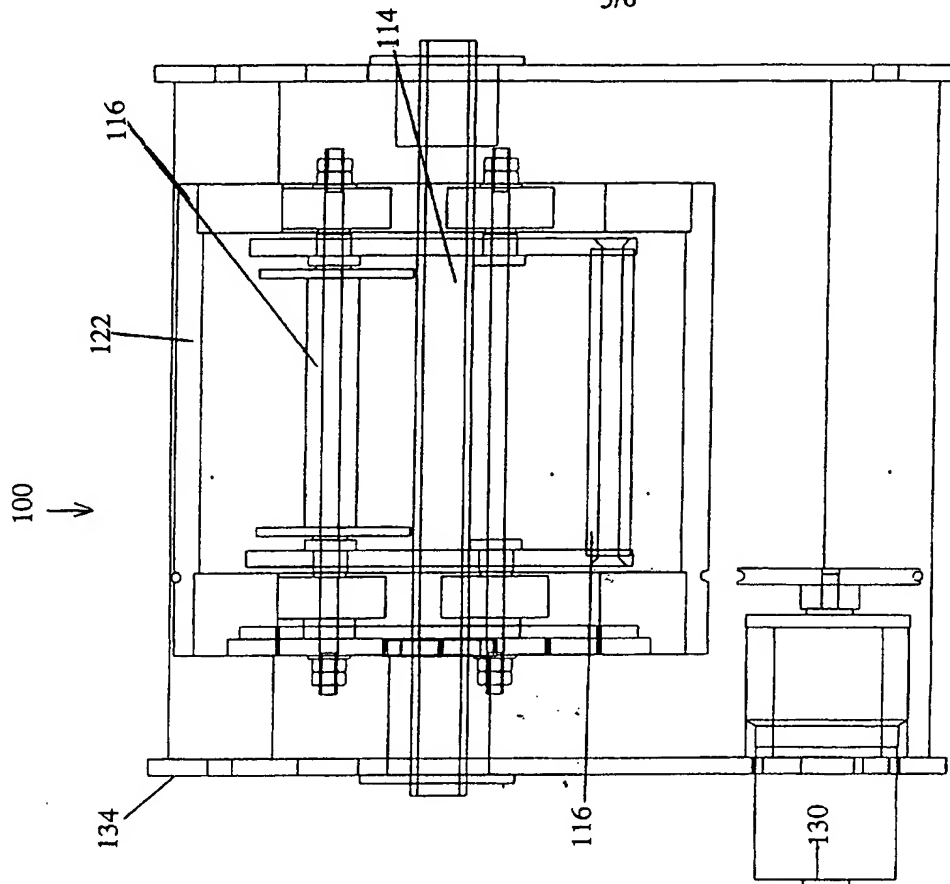


Figure 6

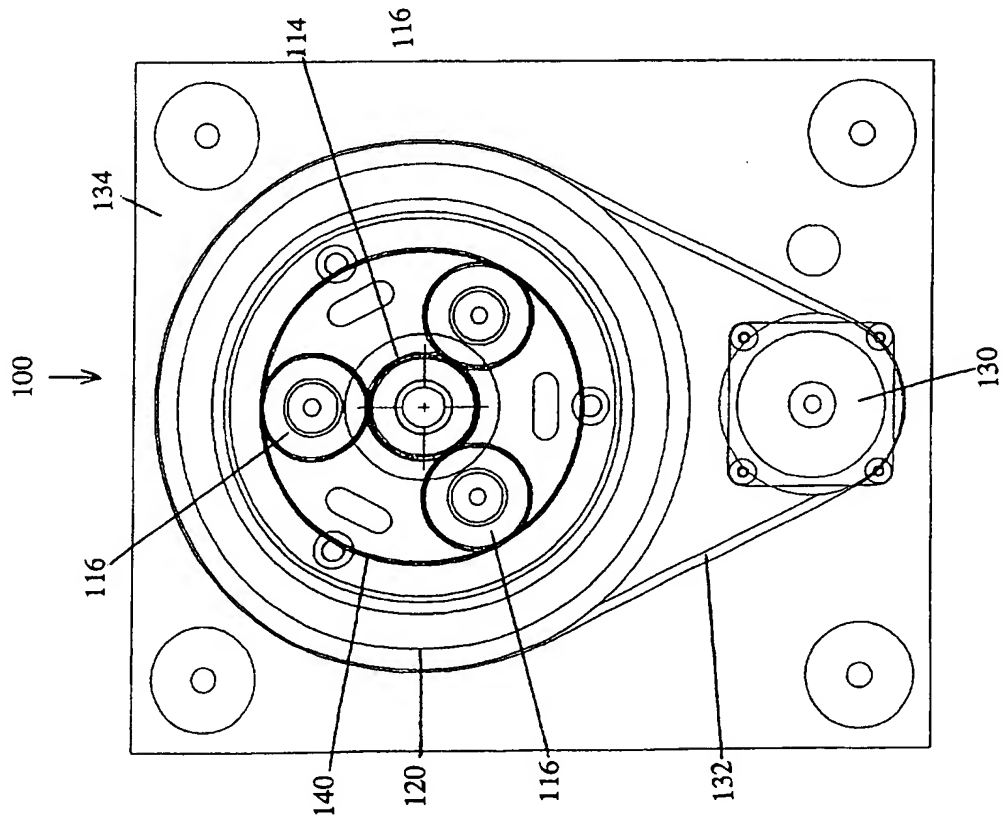


Figure 5

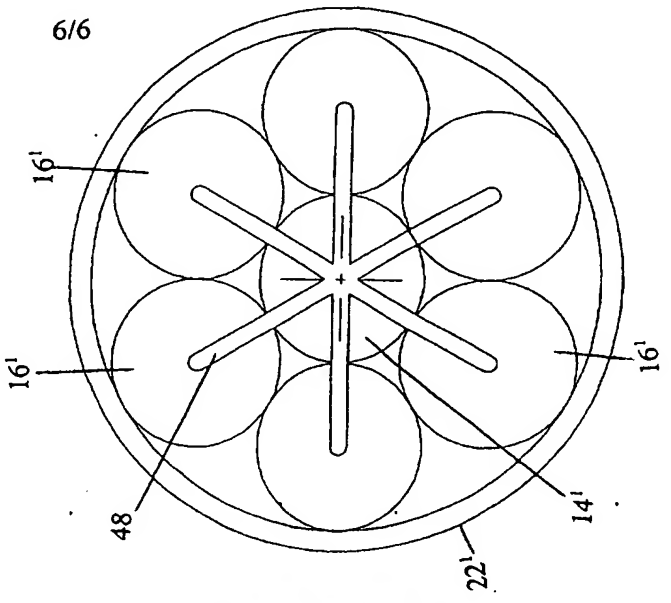
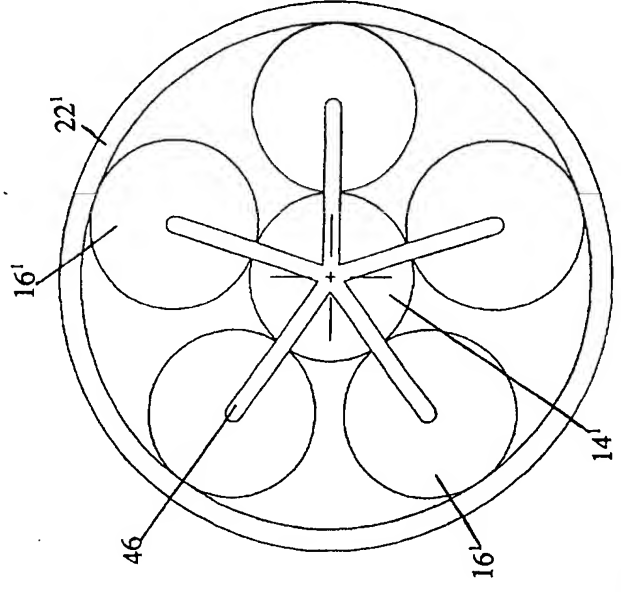
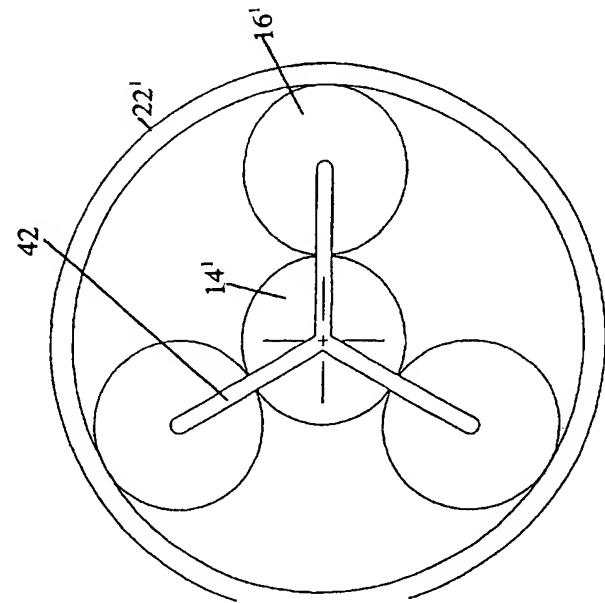
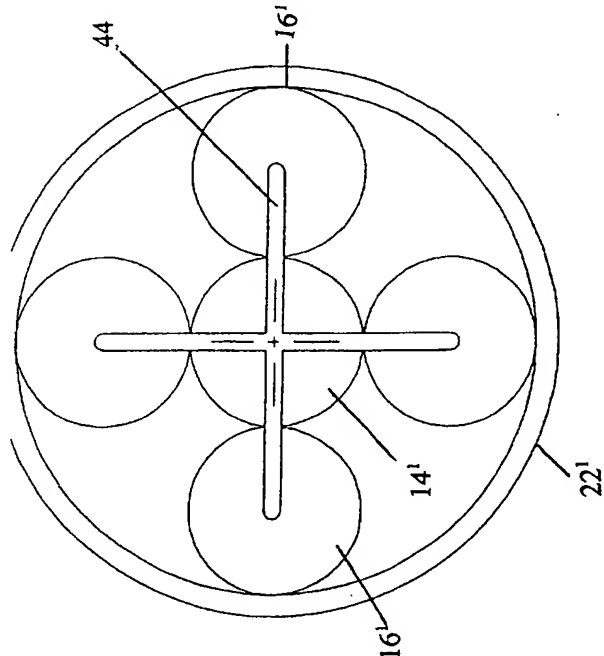
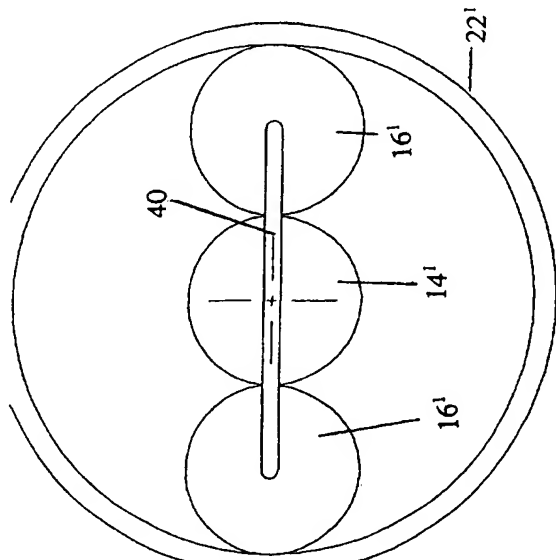


Figure 7

CENTRIFUGE

The present invention relates to a centrifuge.

A current design of centrifuge has a stationary sun gear about which bobbins rotate in a similar manner to that of the planets around the sun. The bobbins are placed in a framework called the rotor, which ensures that the bobbins can rotate about the sun gear. Attached to each bobbin is a gear which meshes with the sun gear. The flying leads are used to transfer the chromatography fluids from the stationary surroundings to the rotating bobbins, where the chromatography process occurs, and then back to the stationary surroundings for processing or analysis.

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The weight of the bobbins is taken by bobbin bearings placed between the bobbins and the rotor. The bobbin bearings have to rotate freely while operating under very heavy loads. The current type of bearing used is a rolling element bearing. This type of bearing has rolling elements (spheres, cylinders, rollers) which rotate between the races. These rolling elements are separated by an item called a cage.

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A fundamental problem with this design of centrifuge is that the rolling elements and the cages of the bobbin bearings exert large loads upon each other due to tangential acceleration caused by the motion of the bobbins about the sun gear. These loads greatly increase the frictional torque of the bearing above that normally expected, the theoretical frictional torque. Figure 1 compares the theoretical and measured torque values for a current design of J-type planet centrifuge. There is a need to increase the performance of these centrifuges which is achieved by increasing the centripetal acceleration generated. The centripetal acceleration can be increased by either increasing the rotational speed or increasing the planetary radius or a combination thereof. As the centripetal acceleration increases so does the tangential acceleration (the tangential acceleration being a component of the centripetal acceleration) acting between the rolling elements and the cages of the bobbin bearings. This in turn increases the frictional torque generated in the bobbin bearings. Higher performance from these centrifuges can be simply achieved by fitting much more powerful drive motors, however this eventually leads to overheating of the bobbin bearings and their failure. The amount of cooling of the bobbin bearings could be increased; however, this adds complexity

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and weight, the latter aggravating the problem. Increasing the amount of cooling only increases the level of centrifuge performance until the frictional problem of bobbin bearings is reasserted.

5 The present invention seeks to provide an improved centrifuge.

According to an aspect of the present invention, there is provided a centrifuge including central guide shaft, a plurality of bobbins located around the guide shaft and rotatable therearound and a support member around the bobbins and providing a substantially
10 cylindrical inner surface around which the bobbins can rotate and operable to support the bobbins.

The support member provides means to support the bobbins during rotation thereof and can substantially avoid the problems of prior art centrifuges mentioned above.

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In the preferred embodiment the support member is free to rotate. This allows for manufacturing variations in the diameter of the bobbins and the diameter of the inner surface of the support member. However, is possible for there to be a fixed drive ratio between bobbins and the support member if all of these parts are manufactured very
20 accurately.

In an embodiment, the central guide shaft is a rotor, which may be driven to drive the bobbins. In another embodiment, the support member is driven imparting rotation to the bobbins. Where the guide shaft is a rotor the support member may be fixed; while where
25 the support member is rotatable, the guide shaft may be fixed.

There are preferably provided two bobbins, although embodiments have been tested with up to ten bobbins, this not necessarily being the maximum number.

30 The bobbins advantageously have diameters which are substantially identical, preferably within a tolerance of $\pm 0.1\%$, most preferably of $\pm 0.05\%$. With the preferred

embodiment, the actual diameter of the bobbins is not important, solely their relative diameters.

Advantageously, the bobbins are located by plane bearings. This feature, assists in location
5 and guidance of the bobbins. These bearings do not support the weight of the bobbins, the support member is supporting this weight. This arrangement avoids the high frictional torque. Alternatives are a needle roller bearing or a hydrostatic bearing in place of a plane bearing, or any other suitable bearing.

10 Similarly, the support member, when rotatable, can be provided with one or more bearings for location and guidance.

The bobbins rotate in the rotor, there is preferably no gearing between the rotor and the bobbins. The sun gear, that is fixed in space and therefore stationary, meshes with the
15 gears attached the bobbins. The rotor and sun gear have the same central axis. The rotor rotates and the bobbins rotate about the rotor central axis and also about their axis due to the meshing of the sun and bobbin gears.

It is possible with the preferred embodiments to provide speeds of rotation of 1,600 to 3,000
20 rpm and higher, using motors which would only produce 800 rpm speeds with the prior art designs of centrifuge.

An embodiment of the present invention is described below, by way of example only, with
reference to the accompanying drawings, in which:

25 Figure 1 is a graph of frictional torque over rotation speed of a prior art centrifuge of planetary type;

Figure 2 is a schematic diagram in partial cross-section of an embodiment of centrifuge in
30 front elevation;

Figure 3 is a schematic diagram in partial cross-section of the centrifuge of Figure 2 in side elevation;

Figure 4 is a schematic diagram in partial cross-section of the centrifuge of Figure 2 in side elevation;

Figure 5 is a schematic diagram in partial cross-section of another embodiment of centrifuge in front elevation; with the weight of the bobbins (3-off) supported by rollers at each end of a bobbin.

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Figure 6 is a schematic diagram in partial cross-section of the centrifuge of Figure 5 in side elevation; and

Figure 7 shows various possible arrangements of bobbins for the centrifuges of Figures 2 to 6.

Referring to Figures 2 to 4, an embodiment of centrifuge 10 is shown within a casing 12. The principal elements of the centrifuge 10 include a rotor 14 around which a plurality of bobbins 16, two in this embodiment, rotate. Around each bobbin 16 there is wound a tubing (not shown) through which liquid analyte is passed for centrifuging. The tubing and connections into and out of the centrifuge 10 are standard in the art so are not described in detail.

The centrifuge is also provided with a support member 22, in the examples described a drum, which provides an inner surface 24 which is substantially circular cylindrical. The inner surface 24 supports the bobbins 16 as can be seen in particular in Figures 2 and 3. As will be apparent in Figure 2, there may be provided a guide 26 engageable by an outer surface of the bobbins 16 to keep the location of the bobbins 16 relative to the support member 22.

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Each bobbin 16 is provided with a plane bearing 28 which allows the bobbins 16 to move radially to take up any tolerance between them and the inner surface 24, while remaining engaged with the gears 18 and 20. There is also provided (shown in Figure 7) a location support, typically rotatably coupled to the rotor 14, for locating the bobbins 16 relative to one another.

In conventional manner and as can be seen in Figures 3 and 4, the rotor 14 is coupled to a motor 30 by a chain 32 or other suitable drive, which rotates the rotor 14 at the desired speed and thereby to impart rotation to the bobbins 16. These Figures show the arrangement of the plane bearings 28, which allow radial movement of the bobbins 16 to about the inner surface of the drum 22 and yet to retain engagement between gears 18 and 20. Gear 18 is the sun gear which is fixed to item 38 and does not rotate. Rotor 14 passes through the centre of item 38 and gear 18.

Figures 3 and 4 also show a support frame 34 which supports the motor 30, the rotor 14 and, indirectly, the drum 22. Of course, the support frame 34 must be sufficiently rigid to support the assembly even during high speed revolution.

In this embodiment, the drum 22 is freely rotatable and in this respect is guided within the frame 34. For this purpose, in this embodiment the drum 22 is supported by two discs 36 on respective radial bearings 38 fixed to the frame 34. The actual form of the guides and, in this form the actual number of discs and bearings, is a matter of choice in dependence upon the chosen design of centrifuge.

Figures 5 and 6 show another embodiment of centrifuge 100 which includes a driven drum 122, three bobbins 116 and a rotor 114. The bobbins 116 include gears 120 which engage stationary gear 118. Similarly, the gearing 120 of the bobbins 116 engages gearing 140 provided on the drum 122.

A suitable belt 132 or other suitable drive is coupled to a motor 130 to drive the drum 122. A suitable support frame 134 supports the assembly.

In use, both embodiments described above cause rotation of the bobbins 16, 116 around the drum 22, 122 and rotor 14, 114, which creates the centrifugal effect in the tubing (not shown) wound around each bobbin 16, 116. The drum 22, 122 supports the weight of the bobbins 16, 116 during rotation and avoids the radial load normally applied to the bearing of the bobbins and which causes the problems experienced with prior art centrifuges. The plane bearings 28 thus only provide location and guidance and do not take any load.

It will also be apparent that the weight of the bobbins 16, 116 is preferably counter-balanced by their number and location relative to one another, so that there are no resultant radial forces on the assembly. This considerably eases the problems during use of the centrifuge.

As a result of these advantages, considerably higher speeds are achievable with the same power motor. It is also possible to increase the size of the centrifuge without suffering some of the problems which would be experienced with prior art designs.

The bobbins 16, 116 are of very similar dimensions, preferably having diameters which are within about $\pm 0.1\%$ and most preferably within $\pm 0.05\%$ of one another. As a result of the structure of the embodiments, the exact dimensions of the bobbins 16, 116 are not important, with errors being taken up by the plane bearings 28. However, relative match of dimensions is important to ensure no substantial friction is developed by the bobbins seeking to rotate at different speeds.

It will also be apparent, and as shown in Figure 7, that the bobbins 16, 116 are coupled to the rotors by struts intended to retain the position of the bobbins 16, 116 relative to one another.

Figure 7 shows schematically various arrangements of bobbins 16' around a rotor 14' and accommodated within a drum 22'. It also shows the supports 40-48 used to locate the bobbins 16' relative to one another and on which the bobbins 16' are free to rotate and to move radially at least to a certain extent.

Of course, the example with six bobbins 16', as with any arrangement having more than six bobbins 16', the bobbins are smaller to avoid them touching one another. The number of bobbins actually provided will be dependent upon the application and customer requirements.

It will be apparent to the skilled person that the drive mechanism for driving the bobbins 16, 16', 116 is not relevant to the embodiments described herein. The gear drive (J-type) shown could be replaced by a belt/chain (I-type) or any other drive version.

As mentioned above, it is not necessary to have a rotating drum. This could be fixed. Moreover, it would be possible to provide a system in which the supporting surface is fixed and which is provided with a rotating cylinder on which the bobbins bear and which couples to the inner surface of the fixed support by a plurality of roller bearings. This could be in place of the disc 36 and bearing 38 of the first-described embodiment.

In place of phase bearings small diameter rolling element bearings could also be used as any induced frictional torque is proportional to the rolling element bearing's diameter. Hydrostatic bearings could also be used in place of the plane bearing.

CLAIMS

1. A centrifuge including a central guide shaft, a plurality of bobbins located around the guide shaft and rotatable therearound and a support member located around the bobbins and
5 providing a substantially cylindrical inner surface around which the bobbins can rotate and operable to support the bobbins.
2. A centrifuge according to claim 1, wherein the support member is a drum.
- 10 3. A centrifuge according to claim 1 or 2, wherein the support member is free to rotate.
4. A centrifuge according to claim 1, 2 or 3, wherein the central guide shaft is a rotor.
- 15 5. A centrifuge according to claim 4, wherein the rotor is coupled to drive means and is operable to drive the bobbins.
6. A centrifuge according to claim 1, 2 or 3, wherein the support member is rotatable, drive means being coupled to the support member to rotate the support member, thereby to
20 impart rotation to the bobbins.
7. A centrifuge according to any preceding claim, wherein the bobbins are located on plane bearings.
- 25 8. A centrifuge substantially as hereinbefore described with reference to and as illustrated in the accompanying drawings.



Application No: GB 9927589.3
Claims searched: 1-8

Examiner: Jason Scott
Date of search: 17 March 2000

Patents Act 1977
Search Report under Section 17

Databases searched:

UK Patent Office collections, including GB, EP, WO & US patent specifications, in:

UK CI (Ed.R): B2P

Int CI (Ed.7): B04B (1/00, 9/00, 9/08, 9/12, 9/14)

Other: ONLINE: WPI, JAPIO, EPODOC

Documents considered to be relevant:

Category	Identity of document and relevant passage	Relevant to claims
A	GB 2013098 A BIURO PROJEKYOW PRZEMYSLU	
A	GB 1346362 A PECK	
A	WO 97/23297 A1 JORGENSON	

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Y	Document indicating lack of inventive step if combined with one or more other documents of same category.	P	Document published on or after the declared priority date but before the filing date of this invention.
&	Member of the same patent family	E	Patent document published on or after, but with priority date earlier than, the filing date of this application.